

ASSESSMENT OF ENVIRONMENTAL NOISE

6th STREET and SPEAR AVENUE AFFORDABLE HOUSING NOISE REPORT

February 6, 2023

By

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ASSESSMENT OF ENVIRONMENTAL NOISE

1.0 INTRODUCTION

This report evaluates potential impacts associated with the construction and operation noise of the 6th Street and Spear Avenue Affordable Housing project in El Centro, California.

1.1 **Project Description**

The proposed project is a 288 - unit multifamily residential development in El Centro, California. The site is located on the northeast intersection of 6th Street and Spear Avenue. The project consists of four parcels with 72 units residential units per parcel, a clubhouse and 520 on-grade parking spaces. The project site is bounded by Wake Avenue to the north, 4th Street to the east, 6th Street to the west, and undeveloped land to the south. According to the El Centro Zoning Map, the project area is classified as CT (Tourist Commercial).



Figure 1 – Areal Image of the Proposed Project Site



1.2 Characteristics of Noise

Noise is usually defined as unwanted sound and can be an undesirable by-product of society's normal day-to-day activities. Sound becomes unwanted when it interferes with normal activities, causes actual physical harm, or has an adverse effect on health.

People judge the relative magnitude of sound sensation in subjective terms such as "noisiness" or "loudness." However, the sound pressure magnitude can be objectively measured and quantified using a logarithmic ratio of pressures which yields the level of sound, utilizing the measurement scale of decibels (dB). The decibel is generally adjusted to the A-weighted level (dBA) which de-emphasizes very low frequencies to better approximate the human ear's range of sensitivity. In practice, the noise level of a sound source is measured using a sound level meter that includes an electronic filter corresponding to the A-weighting curve. Table A.1 in Appendix A of this report defines the decibel along with other technical terms used in this analysis.

Even though the A-weighted scale accounts for the relative loudness perceived by the human ear and, therefore, is commonly used to quantify individual events or general community sound levels, the degree of annoyance or other response effects also depends on several other perceptibility factors, including:

- Ambient (background) sound level
- Magnitude of the event sound level relative to the background noise
- Spectral (frequency) composition (e.g. presence of tones)
- Duration of the sound event
- Number of event occurrences, repetitiveness, and intermittency
- Time of day the event occurs.

In determining the daily level of environmental noise, it is important to account for the difference in human responses to daytime and nighttime noises. At night, exterior background noise levels are generally lower than daytime levels. However, most household noise also decreases at night, and exterior noise may become increasingly noticeable. Further, most people sleep at night and have greater sensitivity to noise intrusion. To account for human sensitivity to nighttime noise levels, a 24-hour descriptor, the Community Noise Equivalent Level (CNEL), has been developed. The CNEL divides the 24-hour day into a daytime period of 7:00 a.m. to 7:00 p.m., an evening period from 7:00 p.m. to 10:00 p.m., and a nighttime period of 10:00 p.m. to 7:00 a.m. In determining the CNEL, noise levels occurring during the evening period are increase by 5 dB, while noise levels occurring during the nighttime periods.



The effects of noise on people fall into three general categories:

- Subjective effects of annoyance and nuisance.
- Interference with activities such as speech, sleep, and learning.
- Physiological effects such as hearing loss.

In most cases, the levels associated with environmental noise produce effects only in the first two categories. However, workers in industrial plants may experience noise effects in the last category. There is no completely effective way to measure the subjective effects of noise or the corresponding reactions of annoyance, because of the wide variation in individual thresholds of annoyance and degrees to which people become acclimated to noise. Thus, an important way of determining a person's subjective reaction to a new noise source is by comparison to the existing environment to which they are accustomed (the "ambient environment"). In general, the more the level of a noise event exceeds the prevailing ambient noise level, the less acceptable the noise source will be to those exposed to it.

With regard to increases in A-weighted noise levels, the following relationships are applicable to this analysis:

- Except in carefully controlled laboratory experiments, a 1 dB change cannot be perceived.
- Outside of a laboratory, a 3 dBA change will be generally perceivable by most people.
- A change in level of at least 5 dBA is considered a noticeable change by most people.
- A 10 dBA change will result in the perception of doubling or halving the loudness of the noise.

Common noise levels associated with various activities are shown on Figure 2, Common Noise Levels.

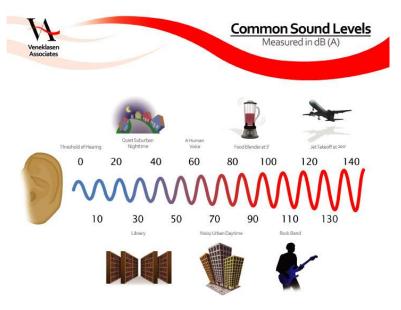


Figure 2 – Common Noise Levels



Noise sources are either "point sources", such as stationary equipment or individual motor vehicles, or "line sources", such as a roadway with a large number of mobile point sources (motor vehicles). Sound generated by a stationary point source typically diminishes (attenuates) at a rate of 6 dBA for each doubling of distance from the source to the receptor at acoustically "hard" sites, and at a rate of 7.5 dBA at acoustically "soft" sites.¹ For example, a 60 dBA noise level measured at 50 feet from a point source at an acoustically hard site would be 54 dBA at 100 feet from the source and it would be 48 dBA at 200 feet from the source. Sound generated by a line source typically attenuates at a rate of 3 dBA and 4.5 dBA per doubling of distance from the source to the receptor for hard and soft sites, respectively.² Man-made or natural barriers can also attenuate sound levels.

The minimum attenuation of exterior to interior noise provided by typical structures is provided in Table 1, Outside to Inside Noise Attenuation.

Building Type	Open Windows	Closed Windows ¹
Residences	17	25
Schools	17	25
Churches	20	30
Hospitals/Convalescent Homes	17	25
Offices	17	25
Theaters	20	30
Hotels/Motels	17	25

Table 1 – Outside to Inside Noise Attenuation (dBA)

Source: Transportation Research Board, National Research Council, Highway Noise: A Design Guide for Highway Engineers, National Cooperative Highway Research Program Report 117.

¹ As shown, structures with closed windows can attenuate exterior noise by a minimum of 25 to 30 dBA.

1.3 Characteristics of Vibration

Vibration is minute variation in pressure through structures and the earth, whereas, noise is minute variation in pressure through air. Some vibration effects can be caused by noise; e.g., the rattling of windows from truck passbys. This phenomenon is related to the coupling of the acoustic energy at frequencies that are close to the resonant frequency of the material being vibrated. Ground-borne vibration attenuates rapidly as distance from the source of the vibration increases. Vibration amplitude can be measured as peak particle velocity (PPV), the maximum

¹ U.S. Department of Transportation, Federal Highway Administration, *Highway Noise Fundamentals*, (Springfield, Virginia: U.S. Department of Transportation, Federal Highway Administration, September 1980), p. 97. A "hard" or reflective site does not provide any excess ground-effect attenuation and is characteristic of asphalt, concrete, and very hard packed soils. An acoustically "soft" or absorptive site is characteristic of normal earth and most ground with vegetation.

² U.S. Department of Transportation, Federal Highway Administration, *Highway Noise Fundamentals*, (Springfield, Virginia: U.S. Department of Transportation, Federal Highway Administration, September 1980), p. 97.



instantaneous peak amplitude in inches per second, or root-mean-square (RMS) velocity in inches per second or as vibration level in decibels (VdB) referenced to 1 micro-inch per second. The ratio between the PPV and the maximum RMS amplitude is termed the "crest factor." According to the Federal Transit Administration (FTA), the PPV level for construction equipment is typically 1.7 to 6 times greater than the RMS vibration level. The FTA uses a crest factor of 4 for the conversion of PPV levels to RMS vibration levels. For the purposes of ground-borne vibration analysis of impacts to existing structures, vibration velocity is described in terms of PPV. For the analysis of the human response to vibration, VdB is utilized.

The vibration velocity threshold of perception for humans is approximately 65 VdB, and a vibration velocity of 75 VdB is the approximate dividing line between barely perceptible and distinctly perceptible levels for many people³. Most perceptible indoor vibration is caused by sources within buildings such as operation of mechanical equipment, movement of people, or the slamming of doors. Typical outdoor sources of perceptible ground-borne vibration are construction equipment, steel-wheeled trains, and traffic on rough roads. Common ground-induced vibrations related to roadway traffic and construction activities pose no threat to buildings or structures. If a roadway is smooth, the ground-borne vibration from traffic is barely perceptible. The range of interest is from approximately 50 VdB, which is typically the background vibration velocity, to 94 VdB. This 94 VdB vibration level corresponds to 0.2 PPV, which is the general threshold where minor damage can occur in non-engineered timber and masonry buildings.

2.0 REGULATORY FRAMEWORK

Many government agencies have established noise regulations and policies to protect citizens from potential hearing damage and various other adverse physiological and social effects associated with noise and ground-borne vibration. The City of El Centro has adopted the Noise Element section, which is based in part on Federal and State regulations and is intended to control, minimize, or mitigate environmental noise effects. The regulations and policies that are relevant to project construction and operation noise are discussed below.

2.1 Applicable State Noise Standards

The State of California has adopted noise compatibility guidelines for general land use planning. The types of land uses addressed by the State standards and the acceptable noise categories for each land use are included in the State of California General Plan Guidelines, which is published and updated by the Governor's Office of Planning and Research. The level of acceptability of the noise environment is dependent upon the activity associated with the particular land use. According to the State, an exterior noise environment up to 65 CNEL is "normally acceptable" for single and multi-family residential uses, up to 75 CNEL is "conditionally acceptable" with special noise insulation

³ – U.S. Department of Transportation, Federal Transit Administration, *Transit Noise and Vibration Impact Assessment*, (Washington, DC: U.S. Department of Transportation, Federal Transit Administration, May 2006), p. 7-8.



requirements, while 75 CNEL and above is identified as "clearly unacceptable" noise levels for residential and hotel uses, respectively.⁴ The maximum allowable interior noise level for residential structures is 45 CNEL.

The California Environmental Quality Act (CEQA) Guidelines establishes guidelines for the evaluation of significant impacts of environmental noise attributable to a proposed project. The guidelines ask whether the project would result in:

- Would the project generate a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?
- 2. Would the project generate excessive ground borne vibration or ground born noise levels?
- 3. For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

2.2 City of El Centro General Plan Noise Element & Municipal Code

The project site is located in the City of El Centro and therefore would potentially affect receptors within the city from onsite and offsite sources. The City Noise Element of the General Plan is a comprehensive program for including noise management in the planning process, providing a tool for planners to use in achieving and maintaining land uses that are compatible with existing and future environmental noise levels. The Noise Policy identifies noise-sensitive land uses and noise sources and defines areas of noise impact for the purpose of developing programs to ensure that residents in El Centro, and other noise sensitive land uses, will be protected from excessive noise intrusion.

As development proposals are submitted to the City, each is evaluated with respect to the provisions in the Noise Element to ensure that noise impacts are reduced through planning and project design. Through implementation of the policies of the Noise Element, El Centro seeks to reduce or avoid adverse noise impacts for the purposes of protecting the general health, safety, and welfare of the community. The most basic planning strategy to minimize adverse impacts on new land uses due to noise is to avoid designating certain land uses at locations within the city that would negatively affect noise sensitive land users. Users such as schools, hospitals, childcare, senior care, congregate care, churches, and all types of residential use should be located outside of any area anticipated to exceed acceptable noise levels as defined by the Land Use Compatibility Matrix or should be protected from noise through sound attenuation measures such as site and architectural design and sound walls. The City of El Centro has

⁴ – State of California, Governor's Office of Planning and Research, *General Plan Guidelines*, (Sacramento, CA: State of California, Governor's Office of Planning and Research, October 2003), p. 250.



adopted guidelines as a basis for planning decisions based on noise considerations. These guidelines are shown in Figure 3.

In the case that the noise levels identified at a proposed project site fall within levels considered normally acceptable, the project is considered compatible with the existing noise environment.

Land Use			Com	munity Noi: (Ldn or C	se Exposure NEL)		
	50	55	60	65	70	75	80
Residential							
Transient Lodging – Motel, Hotel							
Schools, Libraries, Churches, Hospitals, Nursing Homes							
Auditoriums, Concert Halls, Amphitheaters							
Sports Arena, Outdoor Spectator Sports							
Playgrounds, Parks							
Golf Course, Riding Stables, Water Recreation, Cemeteries							
Office Buildings, Business Commercial, and Professional							
Industrial, Manufacturing, Utilities, Agriculture							

Figure 3 – Noise	/Land Use Com	patibility Matrix
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Source: Modified by CBA from 1998 State of California General Plan Guidelines.



ZONE A - Normally Acceptable: Specified land use is satisfactory, based upon the assumption that any buildings involved meet conventional Title 24 construction standards. No special noise insulation requirements.

ZONE B - **Conditionally Acceptable:** New construction or development shall be undertaken only after a detailed noise analysis is made and noise reduction measures are identified and included in the project design.



Zone C- Normally Unacceptable: New construction or development is discouraged. If new construction is proposed, a detailed analysis is required, noise reduction measures must be identified, and noise insulation features included in the design.



ZONE D- Clearly Unacceptable: New construction or development clearly should not be undertaken.



El Centro's quality of life can be reduced by excessive noise levels. The goals, policies and implementation actions of the Noise Element address three major issues related to noise. These include:

- 1) Avoiding the negative effects from noise through the use of land use plaining and noise reduction techniques.
- 2) Minimizing the impact of transportation related noise.
- 3) Minimizing the impact of non-transportation related noise.

Noise and Land Use Planning:

Noise Goal 1: Minimize the effect of noise through proper land use planning

Policy 1.1: Use noise/land use compatibility standards as a guide for the future planning and development decisions.

Policy 1.2: Provide noise control measures and sound attenuating construction in areas of new construction or rehabilitation.

Policy 1.3: Promote alternative sound attenuation measures, such as berms, embankments,

landscaping, setbacks, and architectural design where appropriate, rather than wall barriers.

Policy 1.4: Support changes in the Uniform Building Code that incorporate new technologies

for reducing exterior noise intrusion into structures and the transmission of interior-generated noise within structures.

Transportation Related Noise:

<u>Noise Goal 2</u>: Minimize transportation related noise impacts to preserve the City's overall environment.

Policy 2.1: Reduce transportation related noise impacts to sensitive land uses through the use of noise control measures.

Policy 2.3: Incorporate sound-reduction design in development projects impacted by transportation-related noise. <u>Non-Transportation-Related Noise:</u>

<u>Noise Goal 3</u>: Minimize non-transportation related noise impacts to preserve the City's overall environment.

Policy 3.1: Reduce the impact of noise producing land uses and activities on noise sensitive land uses.

Policy 3.2: Incorporate sound-reduction design in new construction or rehabilitation projects impacted by non-transportation related noise.

Policy 3.3: Require mitigation measures to ensure that noise resulting from public and private construction projects is reduced to an acceptable level.



2.3 City of El Centro Code of Ordinances

The City of El Centro Noise Element establishes noise/land use compatibility criteria. The city uses land use compatibility standards when planning and marking development decisions to ensure that noise producers do not adversely affect sensitive receptors. Per the Section 17.1-4, Table 2 summarizes the City's noise standards for varies type of land uses. The standards represent the maximum acceptable noise levels and are used to determine potential noise impact.

Zone	Time of Day	One hour Average
Single Family Residential Zones	7:00 am – 10:00 pm	50
	10:00 pm – 7:00 am	45
Multi-Family Residential Zone	7:00 am – 10:00 pm	55
	10:00 pm – 7:00 am	50
Commercial Civic and Limited use Zones	7:00 am – 10:00 pm	60
	10:00 pm – 7:00 am	55
Manufacturing Zones	7:00 am – 10:00 pm	75
	10:00 pm – 7:00 am	70

Table 2 – The City of El Centro Noise Standard

Note 1: Zones which exists on the abutting or nearby property at whose boundary the measurement is taken

The sound level limit at a location on a boundary between two (2) zoning districts is the arithmetic mean of the representative limits for the two (2) districts.

If the measured ambient level exceeds the applicable limit shown in the table, the allowable sound level shall be the ambient noise level minus 5 dB but not less than the sound level limit specified in Table 2.

Fixed location public utility distribution or transmission facilities located on or adjacent to a property line shall be subject to the noise limits of this section, measured at or beyond six (6) boundaries of the easement upon which the equipment is located.

According to Section 17.1-8 Construction Equipment, Except for emergency work, it shall be unlawful for any person to operate construction equipment at any construction site, except as outlined in subsections (a) and (b) below:

(a) It shall be unlawful for any person to operate construction equipment at any construction site on Sundays, and days appointed by the president, governor, or the city council for a public holiday. Notwithstanding the above, a person may operate construction equipment on the above specified days between the hours of 10 a.m. and 5 p.m. in compliance with the requirements of subsection (b) of this section at his residence or for the purpose of constructing a residence for himself, provided such operation of construction equipment is not carried on for profit or livelihood. In addition, it shall be



unlawful for any person to operate construction equipment at any construction site on Mondays through Saturdays except between the hours of 6 a.m. and 7 p.m.

(b) No such equipment, or combination of equipment regardless of age or date of acquisition, shall be operated so as to cause noise at a level in excess of seventy-five (75) decibels for more than eight (8) hours during any twenty-four (24) hour period when measured at or within the property lines of any property which is developed and used either in part or in whole for residential purposes.

In the event that lower noise limit standards are established for construction equipment pursuant to state or federal law, said lower limits shall be used as a basis for revising and amending the noise level limits specified in subsection (b) above.

2.4 City of El Centro – Ground-Borne Vibration

The City of El Centro does not establish criteria for maximum vibration thresholds.

The Federal Transit Administration (FTA) provides standards and guidelines for perceptibility and annoyance for ground-borne vibration as well as construction vibration impact criteria for building damage. As discussed in the *Characteristics of Vibration* section above, in most circumstances common ground-induced vibrations related to roadway traffic and construction activities pose no threat to buildings or structures, and for smooth roadways, the ground-borne vibration from traffic is barely perceptible.

The FTA has published a technical manual titled, "Transit Noise and Vibration Impacts Assessment," that provides ground-borne vibration impact criteria with respect to building damage and human response during construction activities. As discussed above, building vibration damage is measured in peak particle velocity described in the unit of inches per second. Table 3, below, provides the Federal Transit Administration vibration criteria applicable to construction activities. According to Federal Transit Administration guidelines, a vibration criterion of 0.20 inch per second should be considered as the significant impact level for non-engineered timber and masonry buildings. Furthermore, structures or buildings constructed of reinforced-concrete, steel, or timber, have vibration damage criteria of 0.50 inch per second pursuant to the FTA guidelines.

Building Category	Peak Particle Velocity (inch per second)	
I. Reinforced-concrete, steel or timber (no plaster)	0.5	
II. Engineered concrete and masonry (no plaster)	0.3	
III. Non-engineered timber and masonry buildings	0.2	
IV. Buildings extremely susceptible to vibration damage	0.12	
Source: Federal Transit Administration, 2006.		

Table 3 - Federal Transit Administration Construction Vibration Impact Criteria for Building Damage



Impacts for the human response to vibration levels are given in VdB by the FTA in Table 8-1 of the *Transit Noise and Vibration Impact Assessment* manual⁵, as shown in Table 4 below. The FTA Land Use Category 1 impact criteria is intended for vibration-sensitive research and manufacturing facilities, hospitals with vibration-sensitive equipment, and university research operations. These Category 1 impact criteria vibration levels are well below those associated with human annoyance but are equal to the threshold of perceptibility. The FTA vibration criteria for Category 2, residential impact, indicate impacts occur at a 72 VdB vibration level for frequent events occurring more than 70 times per day, at 75 VdB for occasional events occurring between 30 and 70 times per day, and at 80 VdB for infrequent events occurring less than 30 times per day.

Land Use Category	GBV Impact Levels (VdB re 1 micro-inch /sec)			
	Frequent Events ¹	Occasional Events ²	Infrequent Events ³	
Category 1 : Buildings where vibration would interfere with interior operations	65 VdB ⁴	65 VdB⁴	65 VdB⁴	
Category 2 : Residences and buildings where people normally sleep	72 VdB	75 VdB	80 VdB	
Category 3 : Institutional land uses with primarily daytime use	75 VdB	78 VdB	83 VdB	
Notes:	•	•	•	

1. "Frequent Events" is defined as more than 70 vibration events of the same source per day. Most rapid transit projects fall into this category.

2. "Occasional Events" is defined as between 30 and 70 vibration events of the same source per day. Most commuter trunk lines have these many operations.

3. "Infrequent Events" is defined as fewer than 30 vibration events of the same kind per day. This category includes most commuter rail branch lines.

4. This criterion limit is based on levels that are acceptable for most moderately sensitive equipment such as optical microscopes. Vibration-sensitive manufacturing or research will require detailed evaluation to define the acceptable vibration levels. Ensuring lower vibration levels in a building often requires special design of the HVAC systems and stiffened floors.

Source: Federal Transit Administration, 2006.

⁵ U.S. Department of Transportation, Federal Transit Administration, *Transit Noise and Vibration Impact Assessment*, (Washington, DC: U.S. Department of Transportation, Federal Transit Administration, May 2006), p. 8-3



2.5 Project Requirements

The above requirements are summarized in the following Table 5.

Activity	Standard	
Residential (General Plan)	Zone A – 50-60 CNEL (Normally Acceptable) Zone B – 60-70 CNEL (Conditionally Acceptable)	
Exterior Noise at Rural & Single-Family Residential Zones (General plan Table N-2)	60 dBA (Outdoor - One hour average)	
Multi- Family Residential Zone (General plan Table N-2)	65 dBA (Outdoor - One hour average)	
Interior Noise at Multi-Family Residences	45 CNEL	
Construction Noise	Prohibited between 7:00 P.M. and 7:00 A.M. Monday thru Saturday, and anytime Sunday and public holidays	
	At Single-family residential property, one-hour average sound level: 55 dBA from 7:00 a.m. to 10:00 p.m. 45 dBA from 10:00 p.m. to 7:00 a.m.	
Operational Noise	At multi-family residential property, one-hour average sound level: 55 dBA from 7:00 a.m. to 10:00 p.m. 50 dBA from 10:00 p.m. to 7:00 a.m.	
	At commercial, civic and limited use zone property, one-hour average sound level: 60 dBA from 7:00 a.m. to 10:00 p.m. 55 dBA from 10:00 p.m. to 7:00 a.m.	
Vibration	At residences where people normally sleep: 72 VdB – greater than 70 events per day. 75 VdB – between 30-70 events per day. 80 VdB – less than 30 events per day.	

Table 5 - Project Requirem	nents
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3.0 ENVIRONMENTAL IMPACTS AND SIGNIFICANCE

3.1 Significance Thresholds

The following significance thresholds are used in this report to evaluate the significance of the project noise impacts:

- Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies.
- Generation of excessive ground borne vibration or ground born noise levels.
- For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels.



3.2 Impact 1. Noise levels in excess of standards

Would the project result in generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies?

3.2.1 Methodology

Analysis of the existing and future noise environments presented in this section is based on technical reports, noise monitoring, and noise prediction modeling. CNEL predictions are based on the measured ambient sound levels and the number of traffic events in a 24-hour period. This was accomplished using the Federal Highway Administration Highway Noise Prediction Model (TNM Version 2.5). The California Department of Transportation (Caltrans) published the "Technical Noise Supplement (TeNS)" in October of 1998 which defines how to predict traffic noise for projects in California. The TeNS, Section N-5520 requires that any traffic noise study conducted after March 30, 2000 utilize the calculation methods used by Federal Highway Administration (FHWA) TNM. This model calculates the average noise level at specific locations based on traffic volumes, average speeds, roadway geometry, and site conditions. The off-site traffic noise is analyzed on an increase in CNEL basis to determine the project's impact.

3.2.2 Existing Ambient Monitored Noise Levels

Traffic on Wake Avenue and 4th Street is the primary noise source around the project site. The land uses surrounding the project are single-family residential, commercial land uses, and parking lots.

According to the Transportation Impact Analysis Report (Ref 3-21-3498) the existing Average Daily Traffic (ADT) count on 4th Street is 14,090 and Wake Avenue reported a total of 9,610.

To establish existing ambient noise levels in areas surrounding the project site, a field monitoring study was conducted. Measurements were performed in and around the project site to document the ambient conditions. Bruel & Kjaer Model 2270 Sound Level Meters, which satisfy the American National Standards Institute (ANSI) for general environmental noise measurement instrumentation, were used for this purpose. Measurements were performed at several locations, as shown on Figure 4. The measurements occurred on November 16, 2022. Noise readings were measured over 1-second intervals with "A" frequency fast time weighting. The weather conditions were normal, and no anomalies were present during the survey periods.

Table 6, Existing Ambient Monitored Noise Levels, provides the noise level data associated with each monitoring period for each location. As shown, noise levels ranged from 53 dBA to 59 dBA, dependent on the road traffic activity and the relative distance between the noise source and the measurement positions.



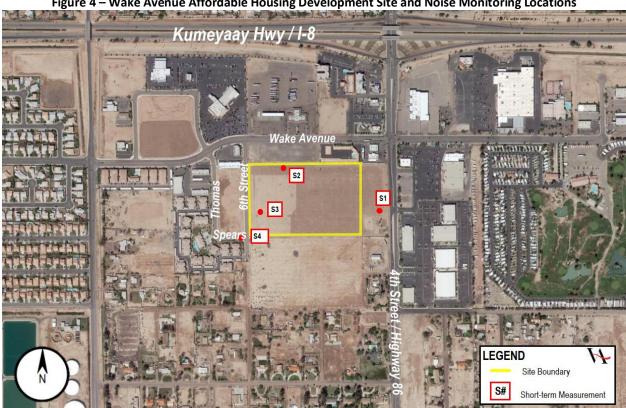


Figure 4 – Wake Avenue Affordable Housing Development Site and Noise Monitoring Locations

Table 6 – Existing Ambient Monitored Noise Levels

Position	Average Sound Level, L _{eq} dBA	Predicted CNEL		
Pos S1	59	62		
Pos S2	58	58		
Pos S3	53			
Pos S4	56			
Notes: Noise measurements taken on November 16, 2022. Source: Veneklasen Associates, 2022.				

Veneklasen also utilized FHWA noise prediction model to predict the existing noise levels at the receivers shown in Figure 4. According to the transportation Impact analysis report dated Feb 24, 2022, the ADT traffic count on 4th Street is 14,090 ADT, and Wake Avenue is 9,610 ADT. Per the Caltrans website the I-8 traffic count in 2020 was 33,000 ADT. Using the above information, the predicted noise levels at S1 location is 62 CNEL, and S2 location is 58 CNEL.



3.2.3 Future Exterior Project Noise Levels

The future traffic conditions for the local roads were not available in the City of El Centro or in the provided Transportation Impact Analysis Report for the project.

Therefore, Veneklasen assumes the yearly traffic increment is 1% and the predicted future traffic count for the Year 2037 on Wake Avenue and 4th Street based on the year 2022 levels are predicted to be 12,318 ADT and 16,811 ADT, respectively. The I-8 predicted future traffic count is approximately 38,637 ADT.

Based on the computer model, the noise level at the S1 (4th Street) and S2 (Wake Avenue) will be 63 CNEL and 59 CNEL, respectively.

The predicted exterior noise levels exceed the General Plan Zone A, Normally Acceptable criteria level for residential zones of CNEL 60, and therefore requires detailed noise analysis and noise reduction measures to be identified and included in the project design as needed. The project should therefore incorporate noise attenuation features such as sound-rated windows into the design.

Mitigation 1. A detailed acoustical analysis of the project should be completed by a qualified acoustical consultant to define the mitigation required such that the exterior and interior noise level requirements are satisfied.

This impact is less than significant with mitigation.

3.2.4 Permanent Increase in Ambient Noise Levels

Increase due to project traffic

A substantial permanent increase in traffic noise would occur if the project would result in an increase of 3 dBA CNEL or more. According to the Traffic Analysis Report, the trip generation due to the project is 1,214 ADT. The report also indicates the project traffic contribution and the total increase of the traffic due to the project contribution plus existing traffic.

The cumulative traffic count on Wake Avenue and 4th Street is 14,480 ADT and 10,610 ADT, respectively. The existing predicted noise level at location S1 is 62 CNEL, and 58 CNEL at location S2.

Based on the computer model, the existing plus project contribution noise levels are predicted to be between 0.1 and 0.4 decibels higher than the existing CNEL level. Therefore, the project traffic contribution is insignificant on 4th Street and Wake Avenue. The summary of the levels for each road is shown in Table 7 below.



Road Segment	Existing Ambient Noise Levels, CNEL	Traffic Model existing plus Project contribution Noise Levels, CNEL	Increase in CNEL	Impact
Wake Avenue	58	58	0.1	Less than Significant
4 th Street	62	62	0.4	Less than Significant

Table 7 – Increase in Ambient Sound Level due to Site-Generated Traffic

The noise levels generated by the site due to traffic causes less than a 3 CNEL increase in the existing ambient levels at the site, and therefore the impact due to project traffic is less than significant.

3.2.5 Operational Noise

The project will include outdoor mechanical equipment, such as split-system outdoor condensing units. Based on published sound power data for units of typical residential size, the noise level will be less than 50 dBA at a distance of 30 feet from the equipment.

The outdoor condensing units for the project will be located on the rooftop of the buildings. A parapet will surround the units with a height that is, at minimum, the height of the units. The residences surrounding the property are one and two-story single or multi-family homes. The nearest residence is approximately 500 feet away, and a motel located north of the site is 85 feet away from the proposed buildings. The predicted mechanical equipment noise level at the nearest receiver, the motel north of the project site, taking into account building elevation and shielding from the parapet, the noise levels due to mechanical equipment has been calculated to be 41 dBA at the nearest residential location. This is significantly below the measured ambient noise level of 58 dBA. These levels are below the operational noise criteria status in Table 6.

This impact is less than significant.

3.2.6 Temporary Increase in Ambient Noise Levels

The construction of the proposed project would increase noise levels in the area. The construction noise impacts were analyzed for long-term noise exposure due to all anticipated construction equipment operating during each phase of construction, as well as for short-term noise exposure from equipment operating along the project site perimeter. Typical construction equipment utilized for each type of activity is indicated in Appendix B. The equipment noise level for all equipment listed for each activity was predicted for each phase in the proposed construction schedule. The equipment used in each construction phase are shown in Table 8.



Phase Name	Equipment Type	Amount	Usage Power	Horsepower	Load Factor
Architectural	Air Compressors	1	6	78	0.48
Coating					
Demolition	Industrial Saws	1	8	81	0.73
Concrete					
Building	Cranes	1	7	231	0.29
Construction					
Demolition	Excavators	3	8	158	0.38
Grading	Excavators	2	8	158	0.38
Building	Forklifts	3	8	89	0.20
Construction					
Building	Generator Sets	1	8	84	0.74
Construction					
Grading	Graders	1	8	187	0.41
Paving	Pavers	2	8	130	0.42
Paving	Paving Equipment	2	8	132	0.36
Paving	Paving Rollers	2	8	80	0.38
Demolition	Rubber Tired Dozers	2	8	247	0.40
Grading	Rubber Tired Dozers	1	8	247	0.40
Site Preparation	Rubber Tired Dozers	3	8	247	0.40
Grading	Scrapers	2	8	367	0.48
Building	Tractors/Loaders/Backhoes	3	7	97	0.37
Construction					
Grading	Tractors/Loaders/Backhoes	2	8	97	0.37
Site Preparation	Tractors/Loaders/Backhoes	4	8	97	0.37
Building	Welders	1	8	46	0.45
Construction					

Table 8 – Proposed Equipment used in Construction Phases

It was assumed that all the equipment is located at the center of the project site and used simultaneously in each phase to represent.

The nearest off-site residential sensitive receivers are located to the west, southwest, and south of the project site. The distance to the property lines of the nearest sensitive receivers from the perimeter of the project site are shown in Table 9.



Receiver	Distance from the Center of the Project Site (feet)	Distance from the Project Property line (feet)
Receiver 1	882	375
Receiver 2	769	115
Receiver 3	1073	710
Receiver 4	852	554
Receiver 5	719	405
Receiver 6	393	25

Table 9 – Distance to the Sensitive Receivers from the Center of Project Site and Property Line

The maximum predicted hourly average noise levels at these sensitive receptors due to construction operations are shown in Table 10 below. Figure 5 shows the location of sensitive receivers adjacent to the site. Appendix B shows the detailed calculation results for the construction equipment noise level at each receiver location.

Receptor	Existing Noise Level at Project Site	Constructio	n Noise Lev		oundaries dBA	of Sensitive	e Receivers,
Receptor	Boundaries, Leq dBA	Rec 1	Rec 2	Rec 3	Rec 4	Rec 5	Rec 6
Demolition		56	57	54	56	58	63
Site Preparation		64	66	63	65	67	72
Grading	53-59	64	65	63	65	66	71
Building Construction	55-59	61	62	59	61	63	68
Architectural Coating		-					
Paving		71	73	70	72	73	79

Table 10 - Construction Noise Levels at the Boundary of Receiver Locations





Figure 5 - Sensitive Receiver Locations

According to the provided equipment list, the construction maximum noise level at Receiver 6 during the paving phase is 79 dBA. According to the City Noise Regulation, there is no decibel criterion for construction noise, and the activities are controlled by limiting the hours of the day for construction. Therefore, for the general compatibility of surrounding sensitive receivers, these activities should be scheduled to limit the number of heavy construction machines operating simultaneously. Additionally, a temporary construction noise barrier is recommended along the north and southwest corner property line of the project site in order to reduce the noise impact to the nearest residential areas.

The barrier is recommended to have a minimum height of 8 feet or more. In order block the line of sight from the noise source to the receiver, the barrier height may be increased. The minimum density of the barrier should be 2 lbs./sq. ft with no holes or gaps.

Mitigation 2. The impact is less than significant with mitigation. The following measures are identified to reduce the potential effects of construction noise on adjacent properties.

- Limit construction activity to the hours listed in Table 5 (6:00 am to 7:00 pm).
- Schedule highest noise-generating activity and construction activity away from noise-sensitive land uses.
- Equip internal combustion engine-driven equipment with original factory (or equivalent) intake and exhaust mufflers which are maintained in good condition.



- Prohibit and post signs prohibiting unnecessary idling of internal combustion engines.
- Locate all stationary noise-generating equipment such as air compressors and portable generators as far as practicable from noise-sensitive land uses.
- Utilize "quiet" air compressors and other stationary equipment where feasible and available.
- Designate a noise disturbance coordinator who would respond to neighborhood complaints about construction noise by determining the cause of the noise complaints and require implementation of reasonable measures to correct the problem. Conspicuously post a telephone number for the disturbance coordinator at the construction site.
- A temporary noise barrier along the north and southwest property line of the project site is recommended. The barrier should have a minimum height of 8 feet or more at some location in order to block the line of sight between the neighbor receptors and the project's construction activities. The noise barrier shall be solid with no gaps or holes and have a minimum density of 2 lbs./sq. ft.

3.3 Impact 2. Excessive ground-borne vibration

Would the project result in exposure of persons to or generation of excessive ground-borne vibration or groundborne noise levels?

Construction equipment associated with building the project would be the only vibration-generating source introduced by the project, as there are no vibration sources from operations that will introduce vibration into the environment. Vibration generated by construction equipment, unless specified otherwise through permitting, would only occur during approved work hours per the City of El Centro, 6:00 am – 7:00 pm, six days a week, excluding holidays. Table 8 shows the equipment used in each construction phase.

Table 11 below, shows the construction equipment proposed by the project planning group and the typical vibration levels generated during operation. It is understood that for this project, pile drivers will not be used. The vibration levels for some of the equipment used in the construction phase are unavailable, and Veneklasen utilized the vibration levels of similar equipment for the analysis.

Equipment	Reference RMS Velocity (Lv) at 25 ft. (VdB)
Vibratory roller	94
Large bulldozer	87
Caisson drilling	87
Loaded trucks	86
Jackhammer	79

Table 11 –Vibration Levels (Lv, VdB) of Typical Construction Equipment at 25 ft



Equipment	Reference RMS Velocity (Lv) at 25 ft. (VdB)
Small bulldozer	58
Source: Federal Transit Administrati	on (except Hanson 2001 for Vibratory rollers), 1995.

Based on the reference vibration levels generated by typical construction equipment and analysis carried out by the Veneklasen, construction equipment vibration levels at the project site boundary will not exceed the criteria per FTA guidelines shown in Table 3.. Therefore, the impact is less than significant, and no mitigation is required. The predicted vibration levels of the proposed construction equipment at the boundary of the project site are shown in Table 12. Appendix B shows the detailed calculation results for the construction equipment vibration level at project boundary.

Receptor	Constr	uction Vib	ration Leve Lv N	-	t Site Bound	daries,
Receptor	Rec 1	Rec 2	Rec 3	Rec 4	Rec 5	Rec 6
Demolition	19	16	23	26	25	23
Site Preparation	25	22	29	32	31	29
Grading	51	48	55	58	57	55
Building Construction	47	44	51	54	53	51
Architectural Coating	-					
Paving	60	56	64	67	66	64

Table 12 – Construction Vibration Levels at the Boundary of Project Site

3.4 Impact 3. Airport noise exposure

For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels?

The project is not within two miles of a public airport or public use airport. Therefore, there is no impact.



4.0 SUMMARY

4.1 Summary of Mitigation Measures

Mitigation 1. A detailed acoustical analysis of the project should be completed by a qualified acoustical consultant to define the mitigation required such that the exterior and interior noise level requirements are satisfied.

Mitigation 2. The impact is less than significant with mitigation. The following measures are identified to reduce the potential effects of construction noise on adjacent properties.

- Limit construction activity to the hours listed in Table 4 (6:00 am to 7:00 pm).
- Schedule highest noise-generating activity and construction activity away from noise-sensitive land uses.
- Equip internal combustion engine-driven equipment with original factory (or equivalent) intake and exhaust mufflers which are maintained in good condition.
- Prohibit and post signs prohibiting unnecessary idling of internal combustion engines.
- Locate all stationary noise-generating equipment such as air compressors and portable generators as far as practicable from noise-sensitive land uses.
- Utilize "quiet" air compressors and other stationary equipment where feasible and available.
- Designate a noise disturbance coordinator who would respond to neighborhood complaints about construction noise by determining the cause of the noise complaints and require implementation of reasonable measures to correct the problem. Conspicuously post a telephone number for the disturbance coordinator at the construction site.
- A temporary noise barrier along the southwest and north property line of the project site is recommended. The barrier should have a minimum height of 8 feet or more at some locations in order to block the line of sight between the neighbor receptors and the project's construction activities. The noise barrier shall be solid with no gaps or holes and have a minimum density of 2 lbs./sq. ft.



4.2 Summary of significance of impacts

	CEQA Noise Impact Question	No Impact	Less Than Significant	Less Than Significant with Mitigation	Potentially Significant
1	Generation of a substantial temporary or permanent increase in ambient noise levels in the vicinity of the project in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies.			X	
2	Generation of excessive ground borne vibration or ground born noise levels.	X			
3	For a project located within the vicinity of a private airstrip or an airport land use plan or, where such a plan has not been adopted within two miles of a public airport or public use airport, would the project expose people residing or working in the project area to excessive noise levels	X			



APPENDIX A

Table A.1 – Definitions of Noise-Related Terms

Term	Definition
Decibel, dB	A unit describing the amplitude of sound equivalent to 20 times the logarithm, to the base 10, of the ratio of the pressure of the sound to the reference pressure of 20 μ Pa.
Frequency, Hz	The number of complete pressure fluctuations per second above and below atmospheric pressure.
A-Weighted Sound Level, dBA	The sound pressure level in decibels as measured in an A-weighting filter network. The A-weighting de-emphasizes the very low frequency components of the sound in a manner similar to the frequency response of the human ear and correlates well with subjective reactions to noise. All sound levels in this report are in the A-weighted scale.
L ₀ (L _{max}), L ₂ , L ₈ , L ₂₅ , L ₅₀	The A-weighted noise levels that are exceeded 0 percent (maximum noise level), 2 percent, 8 percent, 25 percent, and 50 percent of the time during the measurement period.
Equivalent Noise Level, L _{eq}	The average A-weighted noise level during the stated measurement period.
Community Noise Equivalent Level, CNEL	The average A-weighted noise level during a 24-hour day, obtained after addition of 5 decibels in the evening from 7:00 P.M. to 10:00 P.M., and after addition of 10 decibels to noise levels in the night between 10:00 P.M. and 7:00 A.M.
Day-Night Noise Level, DNL, Ldn	The average A-weighted noise level during a 24-hour day, obtained after addition of 10 decibels to levels measured in the night between 10:00 P.M. and 7:00 A.M.
Ambient Noise Level	The composite of noise from all sources near and far. The normal or existing level of environmental noise at a given location.
Impulsive Noise	Sound of short duration. Typically associated with an abrupt onset and rapid decay (i.e., gun-shots, etc.).
Pure Tones	A sound wave, residing over a small range of frequencies, which has a sinusoidal behavior over time.
VdB	Unit of measurement used by FHWA to describe ground-borne vibration. Equivalent to 20 times the logarithm, to the base 10, of the ratio of the root mean square ground-borne velocity to the reference of reference of 1x10 ⁻⁶ in/sec.



APPENDIX B

Table B.1 - Typical Construction Equipment Noise

Equipment Type	FHWA Lmax @ 50 ft.	Usage Factor (%)
Excavator	81	40
Loader	79	40
Grinder	80	40
Rubber Tired Dozer	82	40
Tractor/Loader/Backhoe	84	40
Grader	85	40
Forklifts	84	40
Generator Sets	81	50
Welder	74	40
Paver	77	50
Paving Equipment	82	20
Rollers	80	20
Air Compressors	78	40



Phase	Equipment Type	Unit Amount	Hours/Day	Receiver	Calculated Noise Level at Nearest Sensitive Receptors (Hourly Leq, dBA
				Receiver 1	56
				Receiver 2	57
Building Demolition	Rubber Tired Dozer	2	8	Receiver 3	54
building beinontion		2	°	Receiver 4	56
				Receiver 5	58
				Receiver 6	63
				Receiver 1	64
	Rubber Tired Dozer	3	8	Receiver 2	66
Site Preparation				Receiver 3	63
Site rieparation				Receiver 4	65
	Tractor/Loader/Backhoe	4	8	Receiver 5	67
				Receiver 6	72
	Scrapers	2	8	Receiver 1	64
	Grade	1	8	Receiver 2	65
Grading	Rubber Tired Dozer	1	8	Receiver 3	63
-				Receiver 4	65
	Tractor/Loader/Backhoe	2	8	Receiver 5	66
				Receiver 6	71
	Forklifts	2	<u> </u>	Receiver 1	61
	FUIKIIILS	3	8	Receiver 2	62
Building Construction	Generator Sets	1	8	Receiver 3	59
Building Construction	Tractor/Loader/Backhoe	3	7	Receiver 4	61
	Welder			Receiver 5	63
	weidei	1	8	Receiver 6	68
	Paver	2		Receiver 1	71
	ravel	2	8	Receiver 2	73
Asphalt Paving	Paving Equipment	2		Receiver 3	70
Aspiralt Pavilig	raving Equipment	2	8	Receiver 4	72
	Rollers	2		Receiver 5	73
	NUILEIS	2	8	Receiver 6	79

Table B.2 – Calculated Construction Noise Impacts by Phase



Construction Noise Assessment Results

			Referenc	e Sound Pressure Le	Reference Sound Pressure Level @ 50 ft (dBA re: 20மிa)	(e9h0)		Refere	Reference Utilization (%)	(%)	Receptor R1	ur R1	Receptor R2	ior R2	Receptor R3	tor R3	Recep	Receptor R4	Receptor R5	or R5	Recep	Receptor R6
Equipment	G	Client	FTA	FHWA (Predicted)	FHWA (Predicted) FHWA (Measured)	AN .	Used	Client	FHWA	Used	Distance to R1 Le	Sound Pressure Level @ R1 (dBA re: 20µPa)	Distance to R2 Sound Pressure (ft) re: 20µPa) re: 20µPa)		Distance to R3 (ft)	Sound Pressure Level @ R3 (dBA re: 20µPa)	Distance to R4 (ft)	Sound Pressure Level @ R4 (dBA re: 20µPa)	Distance to RS Sound Pressure (ft) Level @ R5 (dBA re: 20µPa)	Sound Pressure Level @ R5 (dBA re: 20µPa)	Distance to R6 Sound Pressure (ft) tevel @ R6 (dBA re: 20µPa)	Sound Pressure Level @ R6 (dBA re: 20µPa)
Dozer	1	0	85	85	82	0	85	N/A	40%	40%	882	28	769	22	1073	55	852	26	719	8	393	8
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.2	0	393	0
No equipment	1	0	0	0	0	0	V/A	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	Z58	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	Z58	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.1	0	393	0
No equipment	1	0	0	0	0	0	V/N	N/A	N/A	N/A	882	0	769	0	1073	0	258	0	61.1	0	393	0
						Tot	Total Sound Pressure		Level at Receiver NO Barrier	er		56		57		55		56		58		8
						Tota	Total Sound Pressure I	re Level at Recu	Level at Receiver WITH Barrier	'ier		20		50		48		50		51		52

Phase 1 - Demolition

											Pha	se 2 – S	ite Preg	Phase 2 – Site Preparation	_							
			Reference	Sound Pressure Ler	Reference Sound Pressure Level @ 50ft (dBA re: 20µPa)	(eqric		Refere	Reference Utilization (%)	(%)	Recep	Receptor R1	Recep	Receptor R2		Receptor R3	Recep	Receptor R4	Receptor R5	tor R5	Rece	Receptor R6
Equipment	đ	dient	FTA	:HWA (Predicted)	FHWA (Predicted) FHWA (Measured)	VA	Used	Client	FHWA	Used	Distance to R1 (ft)	Sound Pressure Level @ R1 (dBA re: 20µPa)	Distance to R2 (ft)	Distance to R2 Sound Pressure (ft) re: 20µPa)	Distance to R3 (ft)	Sound Pressure Level @ R3 (dBA re: 20µPa)	Distance to R4 (ft)	Sound Pressure Level @ R4 (dBA re: 20µPa)	Distance to R5 (ft)	Sound Pressure Level @ R5 (dBA re: 20µPa)	Distance to R6 Sound Pressure (ft) Level @ R6 (dBA re: 20µPa)	Sound Pressure Level @ R6 (dBA re: 20µPa)
Dozer	2	0	85	85	82	0	85	N/A	40%	40%	882	59	691	09	£201	23	258	29	719	61	E6E	99
Grader	1	0	8	85	0	0	85	N/A	40%	40%	882	95	691	<i>L</i> S	1073	55	258	56	719	58	E6E	89
Scraper	2	0	85	85	58	18	28	N/A	40%	40%	882	62	691	8	£201	09	258	62	719	83	E6E	69
Backhoe	2	0	80	80	78	28	82	N/A	40%	40%	882	35	691	23	1073	झ	852	56	719	28	E6E	89
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	691	0	1073	0	852	0	719	0	E6E	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	691	0	£201	0	258	0	719	0	E6E	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	691	0	£201	0	258	0	917	0	E6E	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	691	0	1073	0	258	0	719	0	E6E	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	691	0	1073	0	852	0	719	0	E6E	0
						Tot	Total Sound Pressu	ire Level at Re	ure Level at Receiver NO Barrier	ier		65		99		63		65		<i>L</i> 9		п
						Tota	Total Sound Pressur	e Level at Reu	ure Level at Receiver WITH Barrier	nier		57		22		ß		57		28		22



28

			Reference	Sound Pressure Le	Reference Sound Pressure Level @ 50 ft (dBA re: 20µ	(edµ0		Referen	Reference Utilization (%)	(%	Receptor R1	orR1	Receptor R2	tor R2	Recep	Receptor R3	Receptor R4	tor R4	Receptor R5	or R5	Recep	Re ceptor R6
Equipment	Ŷð	Client	FTA	FHWA (Predicted)	FHWA (Predicted) HHWA (Measured)	A	Used	Client	FHWA	Used	Distance to R1 L	Sound Pressure Level @ R1 (dBA re: 20µPa)	Distance to R2 (ft)	Sound Pressure Level @ R2 (dBA re:20µPa)	Distance to R3 (ft)	Sound Pressure Level @ R3 (dBA re:20µPa)	Distance to R4 (ft)	Sound Pressure Level @ R4 (dBA re: 20µPa)	Distance to R5 (ff)	Sound Pressure Level @ R5(dBA re: 20µPa)	Distance to R6 (ft)	Sound Pressure Level @ R6(dBA re: 20µPa)
Grader	1	0	85	88	0	0	85	N/A	40%	40%	882	26	769	57	1073	55	852	56	612	58	393	8
Dozer	1	0	85	88	8	0	88	N/A	40%	40%	882	56	769	57	1073	झ	852	56	612	58	393	8
Scraper	2	0	85	85	18	87	87	N/A	40%	40%	882	62	769	8	1073	09	852	62	612	83	393	69
Backhoe	2	0	80	80	82	82	8	N/A	40%	40%	882	56	769	57	1073	15	852	56	6T/	58	393	ន
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	992	0	1073	0	852	0	6T/	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	992	0	1073	0	852	0	719	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	6T.L	0	26E	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	6T/	0	26E	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	992	0	1073	0	852	0	6T/	0	3 9 3	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	992	0	1073	0	852	0	6T/	0	3 9 3	0
						Tot	I Sound Press	Total Sound Pressure Level at Receiver NO Barrier	siver NO Barrie	-		64		99		8		65		99		11
						Total	Sound Pressur	Total Sound Pressure Level at Receiver WITH Barrier	ver WITH Barri	ar		56		ъs		ज		57		57		57

Phase 3 – Grading

										Phase	e 4 – Bu	uilding	Phase 4 – Building Construction	ruction								
			Reference S	iound Pressure Lev	Reference Sound Pressure Level @ 50 ft (dBA re: 20µP	(e,		Reference	Reference Utilization (%)	(5	Receptor R1		Re œ ptor R2	2	Receptor R3		Re ceptor R4		Receptor R5		Receptor R6	82
Equipment		Client	FTA	HWA (Predicted)	FHWA (Predicted) FHWA (Measured)	A	Used	Client	FHWA	Used	Distance to R1 Soun (ft) re	Sound Pressure Dis Level @ R1 (dBA re: 20µPa)	Distance to R2 Sour (ft) re	Sound Pressure Dist Level @ R2 (dBA re: 20µPa)	Distance to R3 Souri (ft) re	Sound Pressure Dist Level @ R3 (dBA re: 20µPa)	Distance to R4 Level (ft) re	Sound Pressure Dista Level @ R4 (dBA re:20µPa)	Distance to RS Sour (ft) re	Sound Pressure Dist Level @ R5 (dBA re: 20µPa)	Distance to R6 Sound Pressure (ft) re: 20µPa)	Sound Pressure Level @ R6 (dBA re: 20µPa)
Front End Loader	8	0	80	80	62	78	80	N/A	40%	40%	882	56	769	57	1073	54	852	55	719	28	33	8
Generator	1	0	82	82	81	76	82	N/A	50%	50%	882	54	769	ß	1073	52	852	ऊ	719	56	333	61
Backhoe	m	0	80	80	82	82	82	N/A	40%	40%	88	28	769	8	1073	56	852	8	719	99	333	8
Welder / Torch	1	0	0	73	74	0	74	N/A	40%	40%	882	45	769	46	1073	43	852	45	719	47	393	25
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	333	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	88	0	92	0	1073	0	852	0	719	0	33	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
						Total S.	Total Sound Pressure Level at Receiver NO Barrier	Level at Recei	ver NO Barrier			61		62		59		19		63		89
												-		1		:		1		:		:
						Total So	Total Sound Pressure Level at Receiver WITH Barrier	e vel at recerv	er WITH Barrie	er.		R		8		51		8		5		55

Veneklasen Associates

	_		Reference	Sound Pressure Le	Reference Sound Pressure Level @ 50 ft (dBA re: 20µPa)	(euha)		Refere.	Reference Utilization (%)	(%)	Receptor R1	or R1	Recep	Receptor R2	Receptor R3	tor R3	Recep	Receptor R4	Recept	Receptor R5	Recep	Receptor R6
Equipment	dty	Client	FTA	FHWA (Predicted)	FHWA (Predicted) FHWA (Measured)	VA	Used	Client	FHWA	Used	Distance to R1 (ft)	Sound Pressure Level @ R1 (dBA re: 20µPa)	Distance to R2 (ft)	Sound Pressure Level @ R2(dBA re: 20µPa)	Distance to R3 (ft)	Sound Pressure Level @ R3 (dBA re: 20µPa)	Distance to R4 (ft)	Sound Pressure Level @ R4 (dBA re: 20µPa)	Distance to R5 (ft)	Sound Pressure Level @ R5 (dBA re: 20µPa)	Distance to R6 (ft)	Sound Pressure Level @ R6 (dBA re: 20µPa)
Paver	2	0	85	8	11	88	88	N/A	50%	50%	882	8	769	55	1073	61	852	8	612	59	38	02
Paver	2	0	85	85	11	88	88	N/A	50%	50%	882	8	692	19	1073	19	258	83	612	99	393	02
Roller	1	0	85	88	80	74	85	N/A	20%	20%	882	8	692	55	1073	15	258	53	612	55	33	09
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	692	0	1073	0	258	0	612	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	692	0	1073	0	258	0	612	0	33	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	692	0	1073	0	258	0	612	0	393	0
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	269	0	1073	0	258	0	6T.L	0	393	0
Pile-driver (Sonic)	1	0	95	0	0	0	95	N/A	N/A	100%	882	02	692	u	1073	89	258	02	612	u	393	ш
No equipment	1	0	0	0	0	0	N/A	N/A	N/A	N/A	882	0	769	0	1073	0	852	0	719	0	393	0
						Tot	I Sound Press	ire Level at Re	Total Sound Pressure Level at Receiver NO Barrier	är		72		73		70		72		73		62
						Total	Sound Pressur	e Level at Rec.	Sound Pressure Level at Receiver WITH Barrier	ier		3		55		62		3		3		3

Phase 6 – Paving

Veneklasen Associates

6th Street and Spear Avenue Affordable Housing Project El Centro, California CEQA Noise Report February 6, 2023



	_				0.5	ΓE	_										
	9	Criteria	Δd	(in/sec)	Ö	vith prima	Lv at R6	23	0	0	0	0	0	0	0	0	0
	Receptor R6			ategory	Reinforced-concre	and uses v	PVequip	5.31E-05	0	0	0	0	0	0	0	0	0
				Building category		titutional	Distance (PPVequip Lv at R6	368	368	368	368	368	368	368	368	368	368
		Criteria	PPV	in/sec)	0.51	nal land us		25	0	0	0	0	0	0	0	0	0
	Receptor R5			tegory	Reinforced-concre	l:Institutio	PVequip	6.74E-05	0	0	0	0	0	0	0	0	0
	2			Building category		Category II	Distance (PPVequip Lv at R5	314	314	314	314	314	314	314	314	314	314
		Criteria	PPV	(in/sec)	0.5 .	nal land u	-v at R4	26	0	0	0	0	0	0	0	0	0
	Receptor R4				. Reinforce d-concre	l:Institutio	Distance (PPVequip	7.29E-05	0	0	0	0	0	0	0	0	0
	2			Building category	. Reinforce	Category II	Distance (298	298	298	298	298	298	298	298	298	298
		Criteria	PPV	(in/sec)	0.5 1.	where vib		23	0	0	0	0	0	0	0	0	0
	Receptor R3				Reinforce d-concre	Buildings	PPVequipLv at R3	5.42E-05	0	0	0	0	0	0	0	0	0
	ľ			Building category		Category I:	Distance (363	363	363	363	363	363	363	363	363	363
on		Criteria	PPV	(in/sec)	0.5	nal land u		15	0	0	0	0	0	0	0	0	0
Phase 1 - Demolition	Receptor R2				ed-concre	l:Institutio	PPVequip	2.24E-05	0	0	0	0	0	0	0	0	0
1-D	ľ			Building category	0.5 I. Reinforced-concre	Category I	Distance (PPVe quip Lv at R2	654	654	654	654	654	654	654	654	654	654
Phase		Criteria	PPV	(in/sec)	0.5	land uses	Lv at R1	19	0	0	0	0	0	0	0	0	0
	Receptor R1			category	ced-concrete,	III:Institutional land uses Category III:Institutional land d Category I: Buildings where vit Category III:Institutional land d Category III:Institutional land uses with primar	PPVequip at I	3.28488E-05	0	0	0	0	0	0	0	0	0
				Building cat			-	507	507	507	507	507	507	507	507	507	507
				<u> </u>	Damage dI. Reinfo	Annoyand Category	v at 25ft (E	58	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
					1		PVref at I	0.003			N/A I	N/A I	N/A I	N/A I	N/A I	N/A I	
							Equipment type PPVref at Lv at 25ft Distance	mall bulldozer	No Equipment N/A	No Equipment N/A	No Equipment	No Equipment	No Equipment	No Equipment	No Equipment	No Equipment	No Equipment N/A
							Annoyance Criteria	Occasional Events: 30-70 events per day Small bulldozer	Frequent Events: >70 events per day	nfrequent Events: <30 events per day	nfrequent Events: <30 events per day	Frequent Events: >70 events per day	Frequent Events: >70 events per day	Frequent Events: >70 events per day			
							An	Occasional Ev	Frequent Eve	Frequent Eve	Frequent Eve	Frequent Eve	Infrequent Ev	Infrequent Ev	Frequent Eve	Frequent Eve	Frequent Ever

		_			0.5	arl											
	9	Criteria	νqq	(in/sec)	0	vith prim	Lv at R6	23	23	23	23	0	0	0	0	0	0
	Receptor R6			ategory	d-concre	and uses v	PVequip	5.31E-05	5.31E-05	5.31E-05	5.31E-05	0	0	0	0	0	0
				Building category	0.5 I. Reinforced-concre	itutional la	Distance (PPVequip Lv at R6	368	368	368	368	368	368	368	368	368	368
		Criteria	PPV	(in/sec) I	0.5 I.	Annoyand Category III:Institutional land usef Category III:Institutional land UCategory I: Buildings where wit Category III:Institutional land utstutional utstutional land uts	i –	25	25	25	25	0	0	0	0	0	0
	Receptor R5	ō	<u> </u>		-concre	nstitution	VequipLv	6.74E-05	6.74E-05	6.74E-05	6.74E-05	0	0	0	0	0	0
	Rec			Building category	0.5 I. Reinforced-concre	tegory III:I	Distance (PPVequipLv at R5	314 6.	314 6.	314 6.	314 6.	314	314	314	314	314	314
		Criteria	>	(in/sec) Bu	0.5 I.F	I land u Ca		26	26	26	26	0	0	0	0	0	0
	Receptor R4	Crit	Δd		concre	stitutiona	/equip Lv a	7.29E-05	7.29E-05	7.29E-05	7.29E-05	0	0	0	0	0	0
	Rece			Building category	0.5 I. Reinforced-concre	egory III:In	Distance (PPVequip Lv at R4	298 7.2	298 7.2	298 7.2	298 7.2	298	298	298	298	298	298
		eria			0.5 I. Re	re vibCate		23 23	23 23	23 23	23 23	0 2	0 2	0 2	0 2	0 2	0 2
	Receptor R3	Criteria	ΡΡV	ry (in/sec)	oncre	dings whe	Distance (PPVequip Lv at R3	5.42E-05 2	5.42E-05 2	5.42E-05 2	5.42E-05 2	0	0	0	0	0	0
	Recep			Building category	nforced-cc	ory I: Buil	nce (PPVe	363 5.42									
n		a			0.5 I. Reinforced-concre	nd uCateg			363	363	363	363	363	363	363	363	363
baratio	r R2	Criteria	ΡΡV	(in/sec)		utional la	Distance (PPVe quip Lv at R2	05 15	05 15	05 15	05 15	0	0	0	0	0	0
e Prep	Receptor R2			Building category	0.5 I. Reinforced-concre	'y III:Instit	e (PPVeq	2.24E-05	2.24E-05	2.24E-05	2.24E-05	0	0	0	0	0	0
– Site				Building	5 I. Reinfo	es Categor		654	654	654	654	654	654	654	654	654	654
Phase 2 – Site Preparation		Criteria	PPV	(in/sec)		al land use	Lv at R1	19	19	19	19	0	0	0	0	0	0
Ч	Receptor R1			gory	nforced-concrete,	nstitution	Vequip at	3.28488E-05	3.28488E-05	3.28488E-05	3.28488E-05	0	0	0	0	0	0
	1 az			ilding category	teinforced	tegory III:I	stance (PP	507 3.	507 3.	507 3.	507 3.	507	507	507	507	507	507
				Build	Damage d I. Reii	noyand Cat	at 25ft (Dis	58	58	58	58	7	7	7	1	7	
					Dai	An	ref at Lv ;	0.003	0.003	0.003	0.003	N/A	N/A	N/A	N/A	N/A	N/A
							PPV	er	er	er	er	t N/A	t N/A	t N/A	t N/A	t N/A	t N/A
							Equipment type PPVref at Lv at 25ft Distance (PPVequip at Lv at R1	Small bulldozer	Small bulldozer	Small bulldozer	Small buildozer	No Equipment	No Equipment	No Equipment N/A	No Equipment N/A	No Equipment	No Equipment
							ш	r day Sr									
							iteria	Occasional Events: 30-70 events per day	Frequent Events: >70 events per day	Infrequent Events: <30 events per day	Infrequent Events: <30 events per day	Frequent Events: >70 events per day	Frequent Events: >70 events per day	Frequent Events: >70 events per day			
							Annoyance Criteria	s: 30-70	>70 eve	- <mark>>70 eve</mark>	>70 eve	- <mark>>70 eve</mark>	s: <30 ev	s: <30 ev	- <mark>>70 eve</mark>	-70 eve	->70 eve
							Anno	<mark>nal Event</mark>	t Events:	t Events:	t Events:	t Events:	ant Event	ent Event	t Events.	it Events:	it Events:
								Occasion	Frequen	Frequen	Frequen	Frequen	Infreque	Infreque	Frequen	Frequen	Frequen
32					-												



eria	sec)	0.5	rimarl	3 6	2	2	3	3	0	0	0	0	0	0
Ē		e	es with p	ip Lv at F										
	category	ced-conc	land use	PPVequ	0.00157	0.00157	5.31E-0	5.31E-0	0	0	0	0	0	c
	Building	. Reinford	titutional	Distance (368	368	368	368	368	368	368	368	368	368
iteria	n/sec)	5	al land us		54	54	25	25	0	0	0	0	0	U
5 8		d-concre	Institution	PVequip Lv	001999	001999	5.74E-05	5.74E-05	0	0	0	0	0	c
	uilding cat	Reinforce	ategory III:	istance (P	314 0	314 0	314 (314 (314	314	314	314	314	31/
iteria	ec)	0.5	al land uC		55	55	26	26	0	0	0	0	0	U
58		-concre	nstitution	Vequip Lv	002163	002163	29E-05	29E-05	0	0	0	0	0	0
	ilding cate	Reinforced	tegory III:I	stance (PP	298 0.	298 0.	298 7.	298 7.	298	298	298	298	298	200
iteria V	sec)	0.5 1. F	here vib Ca		52	52	23	23	0	0	0	0	0	c
5		-concre	uildings wh	Vequip	001609	001609	42E-05	42E-05	0	0	0	0	0	c
	ilding cate	Reinforced	tegory I: Bu	stance (PP	363 0.(363 0.(363 <mark>5</mark> .	363 <mark>5</mark> .	363	363	363	363	363	363
iteria v		0.5 1. F	al land u Ca		44	44	15	15	0	0	0	0	0	c
58		-concre	nstitutione	Vequip Lv	000665	000665	24E-05	24E-05	0	0	0	0	0	c
	ilding cate	Reinforced	tegory III:	stance (PP	654 <u>0.(</u>	654 0.0	654 2.	654 2.	654	654	654	654	654	REA
iteria V		0.5 1. 1	nd uses Ca		48	48	19	19	0	0	0	0	0	c
58		rrete,	stitutional la	'equip at Lv	00974514	00974514	8488E-05	8488E-05	0	0	0	0	0	0
	lding categ	einforced-	_		507 0.00	507 0.00	507 3.2	507 3.2	507	507	507	507	507	507
	Bui	nage d I. R	oyand Cat	t 25ft Dis	87	87	58	58						
		Dan	Ann	refat Lva	0.089	0.089	0.003	0.003						N/0
				/pe PPV		er								+ N/A
				Equipment ty	Large Bulldoz	Large Bulldoz	Small bulldoz	Small bulldoz	<mark>No Equipmen</mark>	No Equipmen	<mark>No Equipmen</mark>	<mark>No Equipmen</mark>	<mark>No Equipmen</mark>	No Fauinment
				Annoyance Criteria										Ereniient Events: >70 events ner dav
	sria Criteria Criteria Criteria Criteria C pov pov pov pov	Criteria Criteria Criteria Criteria Criteria PPV PPV PPV PPV PPV (in/sec) Building category (in/sec) Building category (in/sec) Building category (in/sec) Building category	cria Criteria Criteria Criteria Criteria PPV PPV PPV PPV sec) Building category (in/sec) Building category (in/sec) 0.51. Reinforced-concrel 0.51. Reinforced-concrel 0.51. Reinforced-concrel 0.51. Reinforced-concrel	Criteria Criteria Criteria Criteria Criteria PPV PPV PPV PPV PPV Information PPV PPV PPV PPV State PPV PPV PPV PPV PPV Cateria PPV PPV PPV PPV PPV PPV category (in/sec) Building category (in/sec) Building category (in/sec) Building category (in/sec) cad-concrete	Equipment type PPV Criteria PPV <	Image: spectage Criteria Criteria		ImageCriteria<	ImageCriteria<	ImageCiteria <th< td=""><td>ImageCriteria<</td><td>ImageCiteria<th< td=""><td>Image: bit is a problem with the properties of the properties of the properies of the prope</td><td></td></th<></td></th<>	ImageCriteria<	ImageCiteria <th< td=""><td>Image: bit is a problem with the properties of the properties of the properies of the prope</td><td></td></th<>	Image: bit is a problem with the properties of the properties of the properies of the prope	

Phase 3 – Grading

	Receptor R4	
[]	Receptor R3	
ng Construction	Receptor R2	
Phase 4 – Building Construction	Receptor R1	

RG	Criteria	Δdd	(in/sec)	0.5	vith primarl	Lv at R6	23	51	0	0	0	0	0	0	0	c
Receptor R			Building category	Reinforced-concre	stitutional land use Category III:Institutional land dCategory I: Buildings where vitCategory III:Institutional land dCategory III:Institutional land uses with primar	PPVequip Lv at R6	5.31E-05	0.001346	0	0	0	0	0	0	0	c
			Building		ustitutional	Distance (368	368	368	368	368	368	368	368	368	070
R5	Criteria	νч	(in/sec)	e 0.5 I	tional land	ip Lv at R5	5 25	7 53	0	0	0	0	0	0	0	c
Receptor R5			Building category	Reinforced-concre	y III:Institu	Distance (PPVequip Lv at R5	6.74E-05	0.001707	0	0	0	0	0	0	0	c
	_			0.5 I. Reinfo	d y Categor		314	314	314	314	314	314	314	314	314	110
or R4	Criteria	ΡΡV	/ (in/sec)		tutional lan	Distance (PPVequip Lv at R4	05 26	847 54	0	0	0	0	0	0	0	c
Receptor R4			Building category	. Reinforced-concre	ory III:Instit	nce (PPVeq	3 7.29E-05	3 0.001847	0	8	8	8	0	8	8	•
				0.5 I. Rein	vibCatego		298	298	298	298	298	298	298	298	298	000
r R3	Criteria	٨dd	(in/sec)		ngs where	PPVequip Lv at R3	05 23	74 51	0	0	0	0	0	0	0	c
Receptor R3			Building category	0.5 I. Reinforced-concre	ry I: Buildi	(5.42E-05	0.001374	0	0	0	0	0	0	0	c
				0.5 I. Reinf	d y Catego	Distance	363	363	363	363	363	363	363	363	363	CJC
R2	Criteria	ΡΡΛ	(in/sec)		tional lan	ip Lv at R2	5 15	8 43	0	0	0	0	0	0	0	0
Receptor R2			Building category	Reinforced-concre	r III:Institu	Distance (PPVequip Lv at R2	2.24E-05	0.000568	0	0	0	0	0	0	0	c
			Building	0.5 I. Reinfo	esCategon	Distance	654	654	654	654	654	654	654	654	654	614
L	Criteria	ΡΡV	(in/sec)		al land us	t Lv at R1	5 19	9 47	0	0	0	0	0	0	0	c
Receptor R1			ategory	ce d-concrete,	-	PPVequip at	3.28488E-05	0.000832169	0	0	0	0	0	0	0	c
			Building category	Damage dI. Reinforced-(Annoyand Category III:I	Distance	507	507	507	507	507	507	507	507	507	207
				Damage C	Annoyand	Lv at 25ft	58	86	N/A	N/A	N/A	N/A	N/A	N/A	N/A	NI / V
						PPVref at	0.003	0.076	N/A	N/A	N/A	N/A	N/A	N/A	N/A	NI / N
						Equipment type PPVref at Lv at 25ft Distance (PP	Small buildozer	Loaded trucks	No Equipment	No Equipment	No Equipment	No Equipment	No Equipment	No Equipment	No Equipment	No Equipmont
						Annoyance Criteria	Occasional Events: 30-70 events per day Small bulldozer	Frequent Events: >70 events per day	nfrequent Events: <30 events per day	nfrequent Events: <30 events per day	Frequent Events: >70 events per day	Frequent Events: >70 events per day	Eroditont Eucate: >70 augusts par dau			

						_	Phase 6 – Paving	6 – Pav	ving]										
Building c Damage CI. Reinfor Damage CI. Reinfor Annoyanc Category Annoyanc Category PPVref at Lv at 25ft Distance 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 0.4 0.1/A 10/A 0.1/A 507 0.1/A 10/A 0.1/A 507 0.1/A 10/A 0.1/A 507 0.1/A 10/A					Receptor R1		Rec	ceptor R2	-	Rece	sptor R3		Rece	ptor R4	_	Recep	tor R5		Receptor	R6
Building c bamage d. Reinfor bamage d. Reinfor Annoyanc Category PPVrefat Lv at 25ft Distance 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A S07 N/A N/A N/A N/A N/A S07 N/A N/A						Criteria		Ū	riteria		Crit	teria		Crit	eria		Criteri			Criteria
Building c bamage d: Reinfor bamage d: Reinfor Annoyanc Category PPVrefa t.v at 25ft pistance 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A S07 N/A N/A N/A N/A N/A S07 N/A N/A						PPV		ä	ΡV		١dd			١dd			٨dd			Δd
Damage Cl. Reinfor Annoyand Category PPVrefat Lv at 25ft Distance 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.21 94 0.7 0.7 0.8 0.7 0.1 0.4 0.1 0.1 0.1 0.7 0.1 0.7 0.1 0.7 0.1 0.1 0.1 0.1 0.1 0.7				Building ca			Suilding cat			uilding cate			ding categ	-		ling catego	-		ig category	(in/sec)
Annoyand Category PPVrefat Lvat 25ft Distance I 0.21 94 507 0.21 94 507 0.21 94 507 0.21 94 507 0.21 94 507 0.21 94 507 0.21 94 507 0.21 0.4 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507 0.4 0.7 507			Damage C	I. Reinforce	d-concrete,	0.5	. Reinforcec	d-concre	0.5 .	Reinforced-	concre	0.5 I. R	inforced-	oncre	0.5 I. Re	inforced-co			orced-concre	0.5
Prvetrat Lvat 25t Distance PeVequip Lvat 15t Distance			Annoyand		l:Institutional	land uses C	Category III:	Institution	val land uC.	ategory I: Bu	ildings wh	ere vib Cat	agory III:In	stitutional	land u Cate	gory III:Inst	itutional lar	id ustitution	al land uses	with primarl
0.1 0.1 0.00139 55 6.4 0.00157 51 6.3 0.003396 59 2.98 0.00139 6.1 6.86 0.007318 0.11 0.10 0.0013941 55 6.4 0.00157 51 6.0 0.00139 6.1 6.14 6.16 6.86 0.00318 0.11 0.10 0.00139415 55 6.4 0.00157 51 6.0 0.00139 61 610 <	type.	PPVref at	Lv at 25ft)	PPVequip at [I		Distance (PI	PVequip Lv		istance (PP	Vequip Lv 8		ance (PPV	equip Lv a		ince (PPVe	quip Lv at R		e (PPVequip	Lv at R6
0.21 94 507 0.00229415 55 64 0.00157 51 53 0.003796 59 298 0.005103 62 363 0.003718 51 500 50 <td>oller</td> <td></td> <td></td> <td>507</td> <td>0.002299415</td> <td>55</td> <td></td> <td>0.00157</td> <td>51</td> <td></td> <td>J03796</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>368</td> <td>0.003718</td> <td>59</td>	oller			507	0.002299415	55		0.00157	51		J03796							368	0.003718	59
r 0.21 94 507 0.00279415 55 654 0.0017 51 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 636 0.00718 61 61 636 0.00718 61 61 636 0.00718 61 61 636 0.00718 61 61 61 636 0.00718 61 61 61 636 0.00718 61	oller			507	0.002299415	55		0.00157	51		03796							368	0.003718	59
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